

APPENDICES

APPENDIX A 1 THE GREEK ALPHABET

Alpha	A	α	Iota	I	ι	Rho	P	ρ
Beta	B	β	Kappa	K	κ	Sigma	Σ	σ
Gamma	Γ	γ	Lambda	Λ	λ	Tau	T	τ
Delta	Δ	δ	Mu	M	μ	Upsilon	Y	υ
Epsilon	E	ε	Nu	N	ν	Phi	Φ	ϕ, φ
Zeta	Z	ζ	Xi	Ξ	ξ	Chi	X	χ
Eta	H	η	Omicron	O	\omicron	Psi	Ψ	ψ
Theta	Θ	θ	Pi	Π	π	Omega	Ω	ω

APPENDIX A 2 COMMON SI PREFIXES AND SYMBOLS FOR MULTIPLES AND SUB-MULTIPLES

Factor	Multiple		Factor	Sub-Multiple	
	Prefix	Symbol		Prefix	symbol
10^{18}	Exa	E	10^{-18}	atto	a
10^{15}	Peta	P	10^{-15}	femto	f
10^{12}	Tera	T	10^{-12}	pico	p
10^9	Giga	G	10^{-9}	nano	n
10^6	Mega	M	10^{-6}	micro	μ
10^3	kilo	k	10^{-3}	milli	m
10^2	Hecto	h	10^{-2}	centi	c
10^1	Deca	da	10^{-1}	deci	d

APPENDIX A 3 SOME IMPORTANT CONSTANTS

Name	Symbol	Value
Speed of light in vacuum	c	$2.9979 \times 10^8 \text{ m s}^{-1}$
Charge of electron	e	$1.602 \times 10^{-19} \text{ C}$
Gravitational constant	G	$6.673 \times 10^{-11} \text{ N m}^2 \text{ kg}^{-2}$
Planck constant	h	$6.626 \times 10^{-34} \text{ J s}$
Boltzmann constant	k	$1.381 \times 10^{-23} \text{ J K}^{-1}$
Avogadro number	N_A	$6.022 \times 10^{23} \text{ mol}^{-1}$
Universal gas constant	R	$8.314 \text{ J mol}^{-1} \text{ K}^{-1}$
Mass of electron	m_e	$9.110 \times 10^{-31} \text{ kg}$
Mass of neutron	m_n	$1.675 \times 10^{-27} \text{ kg}$
Mass of proton	m_p	$1.673 \times 10^{-27} \text{ kg}$
Electron-charge to mass ratio	e/m_e	$1.759 \times 10^{11} \text{ C/kg}$
Faraday constant	F	$9.648 \times 10^4 \text{ C/mol}$
Rydberg constant	R	$1.097 \times 10^7 \text{ m}^{-1}$
Bohr radius	a_0	$5.292 \times 10^{-11} \text{ m}$
Stefan-Boltzmann constant	σ	$5.670 \times 10^{-8} \text{ W m}^{-2} \text{ K}^{-4}$
Wien's Constant	b	$2.898 \times 10^{-3} \text{ mK}$
Permittivity of free space	ϵ_0 $1/4\pi \epsilon_0$	$8.854 \times 10^{-12} \text{ C}^2 \text{ N}^{-1} \text{ m}^{-2}$ $8.987 \times 10^9 \text{ N m}^2 \text{ C}^{-2}$
Permeability of free space	μ_0	$4\pi \times 10^{-7} \text{ T m A}^{-1}$ $\cong 1.257 \times 10^{-6} \text{ Wb A}^{-1} \text{ m}^{-1}$

OTHER USEFUL CONSTANTS

Name	Symbol	Value
Mechanical equivalent of heat	J	4.186 J cal^{-1}
Standard atmospheric pressure	1 atm	$1.013 \times 10^5 \text{ Pa}$
Absolute zero	0 K	$-273.15 \text{ }^\circ\text{C}$
Electron volt	1 eV	$1.602 \times 10^{-19} \text{ J}$
Unified Atomic mass unit	1 u	$1.661 \times 10^{-27} \text{ kg}$
Electron rest energy	mc^2	0.511 MeV
Energy equivalent of 1 u	1 u c^2	931.5 MeV
Volume of ideal gas(0 °C and 1atm)	V	22.4 L mol^{-1}
Acceleration due to gravity (sea level, at equator)	g	9.78049 m s^{-2}

ANSWERS

CHAPTER 9

- 9.1** $v = -54$ cm. The image is real, inverted and magnified. The size of the image is 5.0 cm. As $u \rightarrow f$, $v \rightarrow \infty$; for $u < f$, image is virtual.
- 9.2** $v = 6.7$ cm. Magnification = 5/9, i.e., the size of the image is 2.5 cm. As $u \rightarrow \infty$; $v \rightarrow f$ (but never beyond) while $m \rightarrow 0$.
- 9.3** 1.33; 1.7 cm
- 9.4** $n_{ga} = 1.51$; $n_{wa} = 1.32$; $n_{gw} = 1.144$; which gives $\sin r = 0.6181$ i.e., $r \simeq 38^\circ$.
- 9.5** $r = 0.8 \times \tan i_c$ and $\sin i_c = 1/1.33 \simeq 0.75$, where r is the radius (in m) of the largest circle from which light comes out and i_c is the critical angle for water-air interface, Area = 2.6 m²
- 9.6** $n \simeq 1.53$ and D_m for prism in water $\simeq 10^\circ$
- 9.7** $R = 22$ cm
- 9.8** Here the object is virtual and the image is real. $u = +12$ cm (object on right; virtual)
- (a) $f = +20$ cm. Image is real and at 7.5 cm from the lens on its right side.
- (b) $f = -16$ cm. Image is real and at 48 cm from the lens on its right side.
- 9.9** $v = 8.4$ cm, image is erect and virtual. It is diminished to a size 1.8 cm. As $u \rightarrow \infty$, $v \rightarrow f$ (but never beyond f while $m \rightarrow 0$).
 Note that when the object is placed at the focus of the concave lens (21 cm), the image is located at 10.5 cm (not at infinity as one might wrongly think).
- 9.10** A diverging lens of focal length 60 cm
- 9.11** (a) $v_e = -25$ cm and $f_e = 6.25$ cm give $u_e = -5$ cm; $v_o = (15 - 5)$ cm = 10 cm,
 $f_o = u_o = -2.5$ cm; Magnifying power = 20
- (b) $u_o = -2.59$ cm.
 Magnifying power = 13.5.
- 9.12** Angular magnification of the eye-piece for image at 25 cm
 $= \frac{25}{2.5} + 1 = 11$; $|u_e| = \frac{25}{11}$ cm = 2.27 cm; $v_o = 7.2$ cm
 Separation = 9.47 cm; Magnifying power = 88

- 9.13** 24; 150 cm
- 9.14** (a) Angular magnification = 1500
(b) Diameter of the image = 13.7 cm.
- 9.15** Apply mirror equation and the condition:
(a) $f < 0$ (concave mirror); $u < 0$ (object on left)
(b) $f > 0$; $u < 0$
(c) $f > 0$ (convex mirror) and $u < 0$
(d) $f < 0$ (concave mirror); $f < u < 0$
to deduce the desired result.
- 9.16** The pin appears raised by 5.0 cm. It can be seen with an explicit ray diagram that the answer is independent of the location of the slab (for small angles of incidence).
- 9.17** (a) $\sin i'_c = 1.44/1.68$ which gives $i'_c = 59^\circ$. Total internal reflection takes place when $i > 59^\circ$ or when $r < r_{\max} = 31^\circ$. Now, $(\sin i_{\max} / \sin r_{\max}) = 1.68$, which gives $i_{\max} \simeq 60^\circ$. Thus, all incident rays of angles in the range $0 < i < 60^\circ$ will suffer total internal reflections in the pipe. (If the length of the pipe is finite, which it is in practice, there will be a lower limit on i determined by the ratio of the diameter to the length of the pipe.)
(b) If there is no outer coating, $i'_c = \sin^{-1}(1/1.68) = 36.5^\circ$. Now, $i = 90^\circ$ will have $r = 36.5^\circ$ and $i' = 53.5^\circ$ which is greater than i'_c . Thus, *all* incident rays (in the range $53.5^\circ < i < 90^\circ$) will suffer total internal reflections.
- 9.18** (a) Rays converging to a point 'behind' a plane or convex mirror are reflected to a point in front of the mirror on a screen. In other words, a plane or convex mirror can produce a real image if the object is virtual. Convince yourself by drawing an appropriate ray diagram.
(b) When the reflected or refracted rays are divergent, the image is virtual. The divergent rays can be converged on to a screen by means of an appropriate converging lens. The convex lens of the eye does just that. The virtual image here serves as an object for the lens to produce a real image. Note, the screen here is not located at the position of the virtual image. There is no contradiction.
(c) Taller
(d) The apparent depth for oblique viewing decreases from its value for near-normal viewing. Convince yourself of this fact by drawing ray diagrams for different positions of the observer.
(e) Refractive index of a diamond is about 2.42, much larger than that of ordinary glass (about 1.5). The critical angle of diamond is about 24° , much less than that of glass. A skilled diamond-cutter exploits the larger range of angles of incidence (in the diamond), 24° to 90° , to ensure that light entering the diamond is totally reflected from many faces before getting out—thus producing a sparkling effect.
- 9.19** For fixed distance s between object and screen, the lens equation does not give a real solution for u or v if f is greater than $s/4$.
Therefore, $f_{\max} = 0.75$ m.
- 9.20** 21.4 cm

- 9.21** (a) (i) Let a parallel beam be the incident from the left on the convex lens first.
 $f_1 = 30$ cm and $u_1 = -\infty$, give $v_1 = +30$ cm. This image becomes a virtual object for the second lens.
 $f_2 = -20$ cm, $u_2 = + (30 - 8)$ cm = $+22$ cm which gives, $v_2 = -220$ cm. The parallel incident beam appears to diverge from a point 216 cm from the centre of the two-lens system.
- (ii) Let the parallel beam be incident from the left on the concave lens first: $f_1 = -20$ cm, $u_1 = -\infty$, give $v_1 = -20$ cm. This image becomes a real object for the second lens: $f_2 = +30$ cm, $u_2 = -(20 + 8)$ cm = -28 cm which gives, $v_2 = -420$ cm. The parallel incident beam appears to diverge from a point 416 cm on the left of the centre of the two-lens system.

Clearly, the answer depends on which side of the lens system the parallel beam is incident. *Further we do not have a simple lens equation true for all u (and v) in terms of a definite constant of the system (the constant being determined by f_1 and f_2 and the separation between the lenses).* The notion of effective focal length, therefore, does not seem to be meaningful for this system.

- (b) $u_1 = -40$ cm, $f_1 = 30$ cm, gives $v_1 = 120$ cm.
 Magnitude of magnification due to the first (convex) lens is 3.
 $u_2 = + (120 - 8)$ cm = $+112$ cm (object virtual);

$$f_2 = -20 \text{ cm which gives } v_2 = -\frac{112 \times 20}{92} \text{ cm}$$

Magnitude of magnification due to the second (concave) lens = $20/92$.

Net magnitude of magnification = 0.652

Size of the image = 0.98 cm

- 9.22** If the refracted ray in the prism is incident on the second face at the critical angle i_c , the angle of refraction r at the first face is $(60^\circ - i_c)$.
 Now, $i_c = \sin^{-1}(1/1.524) \simeq 41^\circ$
 Therefore, $r = 19^\circ$
 $\sin i = 0.4962$; $i \simeq 30^\circ$

- 9.23** Two identical prisms made of the same glass placed with their bases on opposite sides (of the incident white light) and faces touching (or parallel) will neither deviate nor disperse, but will merely produce a parallel displacement of the beam.

- (a) To deviate without dispersion, choose, say, the first prism to be of crown glass, and take for the second prism a flint glass prism of suitably chosen refracting angle (smaller than that of crown glass prism because the flint glass prism disperses more) so that dispersion due to the first is nullified by the second.
- (b) To disperse without deviation, increase the angle of flint glass prism (i.e., try flint glass prisms of greater and greater angle) so that deviations due to the two prisms are equal and opposite. (The flint glass prism angle will still be smaller than that of crown glass because flint glass has higher refractive index than that of crown glass). Because of the adjustments involved for so many colours, these are not meant to be precise arrangements for the purpose required.