

ANSWERS

Chapter 9

- 9.1** 1.8
- 9.2** (a) From the given graph for a stress of $150 \times 10^6 \text{ N m}^{-2}$ the strain is 0.002
(b) Approximate yield strength of the material is $3 \times 10^8 \text{ N m}^{-2}$
- 9.3** (a) Material A
(b) Strength of a material is determined by the amount of stress required to cause fracture: material A is stronger than material B.
- 9.4** (a) False (b) True
- 9.5** $1.5 \times 10^{-4} \text{ m}$ (steel); $1.3 \times 10^{-4} \text{ m}$ (brass)
- 9.6** Deflection = $4 \times 10^{-6} \text{ m}$
- 9.7** 2.8×10^{-6}
- 9.8** 0.127
- 9.9** $7.07 \times 10^4 \text{ N}$
- 9.10** $D_{\text{copper}}/D_{\text{iron}} = 1.25$
- 9.11** $1.539 \times 10^{-4} \text{ m}$
- 9.12** $2.026 \times 10^9 \text{ Pa}$
- 9.13** $1.034 \times 10^3 \text{ kg/m}^3$
- 9.14** 0.0027
- 9.15** 0.058 cm^3
- 9.16** $2.2 \times 10^6 \text{ N/m}^2$

- 9.17** Pressure at the tip of anvil is 2.5×10^{11} Pa
- 9.18** (a) 0.7 m (b) 0.43 m from steel wire
- 9.19** Approximately 0.01 m
- 9.20** 260 kN
- 9.21** 2.51×10^{-4} m³

Chapter 10

- 10.3** (a) decreases (b) η of gases increases, η of liquid decreases with temperature (c) shear strain, rate of shear strain (d) conservation of mass, Bernoulli's equation (e) greater.
- 10.5** 6.2×10^6 Pa
- 10.6** 10.5 m
- 10.7** Pressure at that depth in the sea is about 3×10^7 Pa. The structure is suitable since it can withstand far greater pressure or stress.
- 10.8** 6.92×10^5 Pa
- 10.9** 0.800
- 10.10** Mercury will rise in the arm containing spirit; the difference in levels of mercury will be 0.221 cm.
- 10.11** No, Bernoulli's principle applies to streamline flow only.
- 10.12** No, unless the atmospheric pressures at the two points where Bernoulli's equation is applied are significantly different.
- 10.13** 9.8×10^2 Pa (The Reynolds number is about 0.3 so the flow is laminar).
- 10.14** 1.5×10^3 N
- 10.15** Fig (a) is incorrect [Reason: at a constriction (i.e. where the area of cross-section of the tube is smaller), flow speed is larger due to mass conservation. Consequently pressure there is smaller according to Bernoulli's equation. We assume the fluid to be incompressible].
- 10.16** 0.64 m s^{-1}
- 10.17** $2.5 \times 10^{-2} \text{ N m}^{-1}$
- 10.18** 4.5×10^{-2} N for (b) and (c), the same as in (a).
- 10.19** Excess pressure = 310 Pa, total pressure = 1.0131×10^5 Pa. However, since data are correct to three significant figures, we should write total pressure inside the drop as 1.01×10^5 Pa.

- 10.20** Excess pressure inside the soap bubble = 20.0 Pa; excess pressure inside the air bubble in soap solution = 10.0 Pa. Outside pressure for air bubble = $1.01 \times 10^5 + 0.4 \times 10^3 \times 9.8 \times 1.2 = 1.06 \times 10^5$ Pa. The excess pressure is so small that up to three significant figures, total pressure inside the air bubble is 1.06×10^5 Pa.
- 10.21** 55 N (Note, the base area does not affect the answer)
- 10.22** (a) absolute pressure = 96 cm of Hg; gauge pressure = 20 cm of Hg for (a), absolute pressure = 58 cm of Hg, gauge pressure = -18 cm of Hg for (b); (b) mercury would rise in the left limb such that the difference in its levels in the two limbs becomes 19 cm.
- 10.23** Pressure (and therefore force) on the two equal base areas are identical. But force is exerted by water on the sides of the vessels also, which has a nonzero vertical component when the sides of the vessel are not perfectly normal to the base. This net vertical component of force by water on sides of the vessel is greater for the first vessel than the second. Hence the vessels weigh different even when the force on the base is the same in the two cases.
- 10.24** 0.2 m
- 10.25** (a) The pressure drop is greater (b) More important with increasing flow velocity.
- 10.26** (a) 0.98 m s^{-1} ; (b) $1.24 \times 10^{-5} \text{ m}^3 \text{ s}^{-1}$
- 10.27** 4393 kg
- 10.28** 5.8 cm s^{-1} , $3.9 \times 10^{-10} \text{ N}$
- 10.29** 5.34 mm
- 10.30** For the first bore, pressure difference (between the concave and convex side) = $2 \times 7.3 \times 10^{-2} / 3 \times 10^{-3} = 48.7$ Pa. Similarly for the second bore, pressure difference = 97.3 Pa. Consequently, the level difference in the two bores is $[48.7 / (10^3 \times 9.8)] \text{ m} = 5.0$ mm.
- The level in the narrower bore is higher. (Note, for zero angle of contact, the radius of the meniscus equals radius of the bore. The concave side of the surface in each bore is at 1 atm).
- 10.31** (b) 8 km. If we consider the variation of g with altitude the height is somewhat more, about 8.2 km.

Chapter 11

- 11.1** Neon: $-248.58 \text{ }^\circ\text{C} = -415.44 \text{ }^\circ\text{F}$;
 CO_2 : $-56.60 \text{ }^\circ\text{C} = -69.88 \text{ }^\circ\text{F}$
- (use $t_F = \frac{9}{5}t_C + 32$)
- 11.2** $T_A = (4/7) T_B$
- 11.3** 384.8 K
- 11.4** (a) Triple-point has a *unique* temperature; fusion point and boiling point temperatures depend on pressure; (b) The other fixed point is the absolute zero itself; (c) Triple-point is 0.01°C , not 0°C ; (d) 491.69.

- 11.5** (a) $T_A = 392.69 \text{ K}$, $T_B = 391.98 \text{ K}$; (b) The discrepancy arises because the gases are not perfectly ideal. To reduce the discrepancy, readings should be taken for lower and lower pressures and the plot between temperature measured versus absolute pressure of the gas at triple point should be extrapolated to obtain temperature in the limit pressure tends to zero, when the gases approach ideal gas behaviour.
- 11.6** Actual length of the rod at $45.0 \text{ }^\circ\text{C} = (63.0 + 0.0136) \text{ cm} = 63.0136 \text{ cm}$. (However, we should say that change in length up to three significant figures is 0.0136 cm , but the total length is 63.0 cm , up to three significant places. Length of the same rod at $27.0 \text{ }^\circ\text{C} = 63.0 \text{ cm}$.)
- 11.7** When the shaft is cooled to temperature -69°C the wheel can slip on the shaft.
- 11.8** The diameter increases by an amount $= 1.44 \times 10^{-2} \text{ cm}$.
- 11.9** $3.8 \times 10^2 \text{ N}$
- 11.10** Since the ends of the combined rod are not clamped, each rod expands freely.
 $\Delta l_{\text{brass}} = 0.21 \text{ cm}$, $\Delta l_{\text{steel}} = 0.126 \text{ cm} = 0.13 \text{ cm}$
 Total change in length $= 0.34 \text{ cm}$. No 'thermal stress' is developed at the junction since the rods freely expand.
- 11.11** $0.0147 = 1.5 \times 10^{-2}$
- 11.12** $103 \text{ }^\circ\text{C}$
- 11.13** 1.5 kg
- 11.14** $0.43 \text{ J g}^{-1} \text{ K}^{-1}$; smaller
- 11.15** The gases are diatomic, and have other degrees of freedom (i.e. have other modes of motion) possible besides the translational degrees of freedom. To raise the temperature of the gas by a certain amount, heat is to be supplied to increase the average energy of all the modes. Consequently, molar specific heat of diatomic gases is more than that of monatomic gases. It can be shown that if only rotational modes of motion are considered, the molar specific heat of diatomic gases is nearly $(5/2) R$ which agrees with the observations for all the gases listed in the table, except chlorine. The higher value of molar specific heat of chlorine indicates that besides rotational modes, vibrational modes are also present in chlorine at room temperature.
- 11.16** 4.3 g/min
- 11.17** 3.7 kg
- 11.18** $238 \text{ }^\circ\text{C}$
- 11.20** 9 min
- 11.21** (a) At the triple point temperature $= -56.6 \text{ }^\circ\text{C}$ and pressure $= 5.11 \text{ atm}$.
 (b) Both the boiling point and freezing point of CO_2 decrease if pressure decreases.
 (c) The critical temperature and pressure of CO_2 are $31.1 \text{ }^\circ\text{C}$ and 73.0 atm , respectively. Above this temperature, CO_2 will not liquefy even if compressed to high pressures.
 (d) (a) vapour (b) solid (c) liquid
- 11.22** (a) No, vapour condenses to solid directly.
 (b) It condenses to solid directly without passing through the liquid phase.

- (c) It turns to liquid phase and then to vapour phase. The fusion and boiling points are where the horizontal line on P - T diagram at the constant pressure of 10 atm intersects the fusion and vaporisation curves.
- (d) It will not exhibit any clear transition to the liquid phase, but will depart more and more from ideal gas behaviour as its pressure increases.

Chapter 12

12.1 16 g per min

12.2 934 J

12.4 2.64

12.5 16.9 J

12.6 (a) 0.5 atm (b) zero (c) zero (assuming the gas to be ideal) (d) No, since the process (called free expansion) is rapid and cannot be controlled. The intermediate states are non-equilibrium states and do not satisfy the gas equation. In due course, the gas does return to an equilibrium state.

12.7 15%, 3.1×10^9 J

12.8 25 W

12.9 450 J

12.10 10.4

Chapter 13

13.1 4×10^{-4}

13.3 (a) The dotted plot corresponds to 'ideal' gas behaviour; (b) $T_1 > T_2$; (c) 0.26 J K^{-1} ; (d) No, $6.3 \times 10^{-5} \text{ kg}$ of H_2 would yield the same value

13.4 0.14 kg

13.5 $5.3 \times 10^{-6} \text{ m}^3$

13.6 6.10×10^{26}

13.7 (a) $6.2 \times 10^{-21} \text{ J}$ (b) $1.24 \times 10^{-19} \text{ J}$ (c) $2.1 \times 10^{-16} \text{ J}$

13.8 Yes, according to Avogadro's law. No, v_{rms} is largest for the lightest of the three gases; neon.

13.9 $2.52 \times 10^3 \text{ K}$